

Ideal Reaktor - Värmebalanser

Reaktioner - endo- eller exoterm

Reaktionshastigheten påverkas av temperaturändringar

$$\dot{Q} = UA(T_a - T)$$

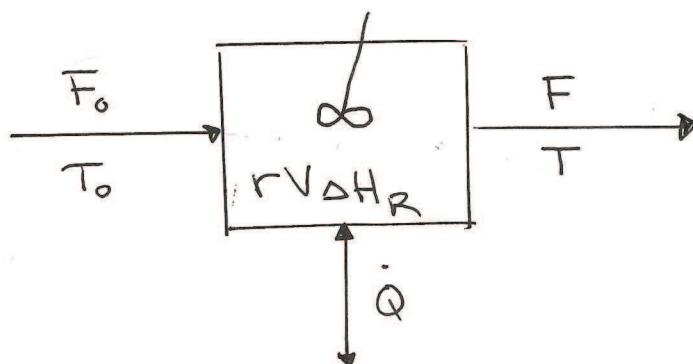
$\left. \begin{array}{l} U - \text{total värmeövert. koeff.} \\ A - \text{värmeövert. Area} \\ T_a = \text{fluid temp.} \\ T = \text{reaktor temp.} \end{array} \right\}$

CSTR:

T_a kan variera ty

$$\dot{Q} = UA \Delta T_{lm} = UA \frac{\Delta T_{A_1} - \Delta T_{A_2}}{\ln\left(\frac{T_{A_1} - T}{T_{A_2} - T}\right)}$$

$$U = \frac{1}{\frac{1}{h} + \frac{1}{k} + \frac{1}{h}}$$



Värmebalans

$$\sum F_{i,0} \int_{T_{ref}}^{T_0} c_{p,i} dT - \sum F_i \int_{T_{ref}}^{T_*} c_{p,i} dT + rV(-\Delta H_R(T_{ref})) + \dot{Q} = \sum N_i \frac{dT}{dt}$$

$T_{ref} = T$:

$$\sum F_{i,0} \int_T^{T_0} c_{pi} dT + rV(-\Delta H_R(T)) + \dot{Q} = \underbrace{\sum N_i \frac{dT}{dt}}_{UA\Delta T_{Im}} = 0 \text{ vid steady-state}$$

Obs! Värmebalansen gäller för en tank reaktor (ideal)

Molbalans (för ideal tank):

$$F_{j,0} - F_j + (\nu_j r)V = 0 \rightarrow rV = \frac{x_j F_{j,0}}{(-\nu_j)}$$

För en batch reaktor gäller värmebalansen för en unsteady tank vid unsteady-state med ändringarna:

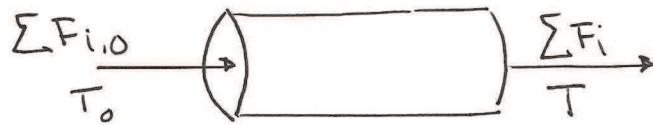
$$\left\{ \begin{array}{l} F_{i,0} = F_i = 0 \\ \sum c_{pi} N_i \frac{dT}{dt} = -rV \Delta H_R(T) + \dot{Q} \end{array} \right. \rightarrow \frac{dT}{dt} = \frac{-rV \Delta H_R(T) + \dot{Q}}{\sum_i N_i c_{pi}}$$

Tubreaktor:

$$\sum F_i \int_{T_{ref}}^T c_{pi} dT - \sum F_i \int_{T_{ref}}^{T+dT} c_{pi} dT - r \Delta H_R(T_{ref}) dV + d\dot{Q} = 0$$

$$\sum F_i c_{pi} \frac{dT}{dV} = r(-\Delta H_R(T)) + U_a (T_a - T)$$

Måste användas om icke-adiab.



$$\sum F_{i,0} \frac{T_0}{T_0} = \sum F_i \frac{T_i}{T_{\text{ref}}} + \sum F_i \left(\frac{x_i F_{i,0}}{(-\Delta f_j)} (-\Delta H_R(T_{\text{ref}})) \right) = 0$$

Ex. Icke-isotermreaktorer



$\Delta H_R = -58.97 \text{ kJ/mol}$ exoterm pga negativ

$C_P \text{gas} = 151 \text{ J/mol}\cdot\text{K}$ kon antas vara konst.

$T:H = 1:1 \text{ mol}$

$F_{T,0} = 1000 \text{ mol/h}$

$$r = K C_H^{0.5} C_T$$

$T = 700^\circ\text{C}$ (973 K)

$P_{\text{tot}} = 40 \text{ atm}$ konstant

$x_T = 0.5$

$K = 1.1 \cdot 10^7 \exp\left(-\frac{E}{RT}\right), E = 213 \text{ kJ/mol}$

(a) Om en adiabatisk tubreaktor används, vilken volym på reaktorn krävs?

$$\frac{dF_T}{dV} = r_T \quad \left\{ F_T = F_{T,0} - x_T F_{T,0} \right\}$$

$$\rightarrow -F_{T,0} \frac{dx_T}{dV} = K C_H^{0.5} C_T$$

$$\int_0^{0.5} dV = F_{T,0} \int_0^{0.5} \frac{dx_T}{k C_H^{0.5} C_T} \quad \left. \begin{array}{l} \\ \end{array} \right\} k = k(T) \text{ dvs ej konst!}$$

$$C_H = y_H \frac{P}{RT} = \underbrace{\frac{F_H}{F_{\text{tot}}}}_{\text{konst.}} \cdot \frac{P}{RT} = \underbrace{\frac{F_{H,0} - F_{H,0}x}{2F_{H,0}}}_{\text{fkn. av utbytet}} \cdot \frac{P}{RT} = F_{H,0} + F_{T,0}$$

$$C_H = (1-x_T) \frac{P}{2RT}$$

$$C_T \equiv C_H \quad \text{ty 1:1 förhållande!}$$

$$\rightarrow V = F_{T,0} \int_0^{0.5} \frac{dx_T}{A \exp(-\frac{E}{RT}) (1-x_T)^{0.5} \cdot \left(\frac{P}{2RT}\right)^{1.5}}$$

Behöver ett förhållande mellan temperatur och utbyte
 \rightarrow Värmebalans!

VB:

$$\sum F_{i,0} \int_{T_{\text{ref}}}^{T_0} c_{pi} dT - \sum F_i \int_{T_{\text{ref}}}^T c_{pi} dT + \frac{x_T F_{T,0}}{(-\gamma_+)} (-\Delta H_R) = 0$$

adiabatisk!

$$\underbrace{2F_{T,0}}_{2F_{T,0}} \cdot c_p (T_0 - T_{\text{ref}}) - F_{T,0} c_p (T - T_{\text{ref}}) + x_T F_{T,0} (-\Delta H_R) = 0$$

$$\cancel{2F_{T,0} c_p (T_0 - T_{\text{ref}})}$$

$$\cancel{2F_{T,0} c_p (T_0 - T)} + x_T F_{T,0} (-\Delta H_R) = 0$$

$$T = \frac{x_T(-\Delta H_R)}{2C_P} + T_0 \quad \text{in i integralen!}$$

$$V = F_{T,0} \int_0^{0.5} I(x_T) dx_T \dots$$

(b) Om vi istället använder en adiabatisk tank, blir volymen större eller mindre?

$$F_{T,0} - F_T + rV = 0$$

$$x_T F_{T,0} - \kappa C_H^{0.5} C_T V = 0$$

$$V = F_{T,0} \frac{x_T}{\kappa C_H^{0.5} C_T} \quad \text{integral samma som i (a)!}$$

$$V = F_{T,0} (I(x=0.5))$$